# **Dissipative effects in mixtures**

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# Comparison of hydrodynamic calculations with experimental data $\rightarrow$ extraction of $\eta$ /s, EoS ...

From  $\eta$ /s we learn about the inner dynamics in the medium

## **Motivation**

Can we apply standard, one-component hydrodynamics to describe dissipative effects in a mixture?



Interaction cross sections  $\sigma_{_{11}}, \sigma_{_{12}}, \sigma_{_{22}}$ 

*Two distinct mean-free path scales* 

QGP or Hadron Gas are mixtures

# **Dissipative hydro**

Ideal hydrodynamics:

 $\partial_{\mu}T^{\mu\nu}=0$   $T^{\mu\nu}$  is isotropic locally  $\leftrightarrow$  Momentum distribution is isotropic  $\partial_{\mu}N^{\mu}=0$ EoS

Israel-Stewart hydrodynamics:



 $\pi^{\mu
u}$  describes anisotropy of the momentum space distribution

- $\partial_{\mu}T^{\mu\nu}=0$  total energy is conserved
- $\partial_{\mu} N^{\mu} = 0$  total particle number is conserved



Same as the standard Israel-Stewart for each mixture component? Then, what is the viscosity of **mixture components**?

For our derivation we assume:

> particle numbers are conserved (no radiative processes)

- >  $T_1 = T_2 = T$  (rather strong assumption, but we really need this one)
- > the global frame  $u^{\mu}$  is not very different from the frames  $u^{\mu}_{i}$  of the components

Need to check these two in transport calculations

For our derivation we assume:

> particle numbers  $N_i$  are conserved (no radiative processes)

>  $T_1 = T_2 = T$  (rather strong assumption, but we really need this one)

> the global frame  $u^{\mu}$  is not very different from the frames  $u^{\mu}_{i}$  of the components

> we take isotropic scatterings,  $d\sigma/d\Omega$  independent of  $\Omega$ 

can translate cross section to viscosity  $\eta = \frac{6}{5} \frac{T}{\sigma}$ 

For two components with a given  $n_1/n_2$  and cross sections  $\sigma_{11}$ ,  $\sigma_{12}$ ,  $\sigma_{22}$ 

$$\dot{\pi}_{1} = -\pi_{1} \cdot \left(\frac{5}{9} n_{1} \sigma_{11} + \frac{7}{9} n_{2} \sigma_{12}\right) + \pi_{2} \cdot \frac{2}{9} n_{1} \sigma_{12} + gradient \quad terms$$
$$\dot{\pi}_{2} = -\pi_{2} \cdot \left(\frac{5}{9} n_{2} \sigma_{22} + \frac{7}{9} n_{1} \sigma_{12}\right) + \pi_{1} \cdot \frac{2}{9} n_{2} \sigma_{12} + gradient \quad terms$$

Two relaxation times per equation Compare with the Israel-Stewart Eq.:

$$\dot{\pi} = -\pi \cdot \frac{5}{9} n\sigma + + gradient \ terms$$

#### Dynamics in a mixture

Let's check the relaxation part of the equations

$$\dot{\pi}_{1} = -\pi_{1} \cdot \left(\frac{5}{9} n_{1} \sigma_{11} + \frac{7}{9} n_{2} \sigma_{12}\right) + \pi_{2} \cdot \frac{2}{9} n_{1} \sigma_{12} + gradient \quad terms$$
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 $n_{1}, n_{2}$   $T_{1} = T_{2} = T$   $\sigma_{11}, \sigma_{12}, \sigma_{22}$   $\pi_{1}, \pi_{2}$ 

$$f_{i} = d \cdot e^{-E/T} \cdot \left( 1 + \frac{3}{8 e_{i} T^{2}} \cdot \pi_{i} \cdot \left( \frac{1}{2} p_{T}^{2} - p_{z}^{2} \right) \right)$$

Grad 's Formalism

**BAMPS BOX** 

#### Mixture in BAMPS



$$n_{1}/n_{2} = 5$$
  
initial  $\pi_{1}/\pi_{2} = n_{1}/n_{2}$   
 $\sigma_{11} = 4 \ mb$   
 $\sigma_{12} = 2 \ mb$ ,  
 $\sigma_{22} = 1 \ mb$   
 $T = 0.4 \ GeV$ 

#### **Relaxation in BAMPS**

In the standard **one-component** Israel-Stewart hydrodynamics:



#### **Green-Kubo**

Application of Green-Kubo formula in BAMPS: C.Wesp et al, arXiv:1106.4306

$$\eta = \frac{V}{T} \int_0^\infty C(\tau) \, d\tau$$

Auto-correlation function

$$C(\tau) = \frac{1}{3} \left| \langle \pi^{xy}(0) \pi^{xy}(\tau) \rangle + \langle \pi^{xz}(0) \pi^{xz}(\tau) \rangle + \langle \pi^{yz}(0) \pi^{yz}(\tau) \rangle \right|$$

 $\tau =$ correlation time

#### Green-Kubo

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#### Mixture in BAMPS



#### Dynamics in a mixture

$$\dot{\pi}_{1} = -\pi_{1} \cdot \left(\frac{5}{9}n_{1}\sigma_{11} + \frac{7}{9}n_{2}\sigma_{12}\right) + \pi_{2} \cdot \frac{2}{9}n_{1}\sigma_{12}$$
$$\dot{\pi}_{2} = -\pi_{2} \cdot \left(\frac{5}{9}n_{2}\sigma_{22} + \frac{7}{9}n_{1}\sigma_{12}\right) + \pi_{1} \cdot \frac{2}{9}n_{2}\sigma_{12}$$



with  $r(\tau) = \frac{\pi_{1}(\tau)}{\pi_{2}(\tau)} = A(n, \sigma) \cdot \tanh(\tau \cdot B(n, \sigma) + C(n, \sigma, \pi_{0}))$   $\lambda_{1}^{-1} = n_{1}\sigma_{11} + n_{2}\sigma_{12} \qquad \lambda_{2}^{-1} = n_{2}\sigma_{22} + n_{1}\sigma_{12}$ 

#### Mixture in BAMPS

$$\eta(\tau) = \frac{2}{5} \cdot e \cdot \left( \frac{r(\tau)}{1 + r(\tau)} \cdot \lambda_1^{-1} + \frac{1}{1 + r(\tau)} \cdot \lambda_2^{-1} \right)$$

,

$$r(\tau) = \frac{\pi_1(\tau)}{\pi_2(\tau)} = A(n, \sigma) \cdot \tanh\left(\tau \cdot B(n, \sigma) + C(n, \sigma, \pi_0)\right)$$



Existence of a characteristic stationary value

#### **Dynamics in mixtures**

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mixture with mean free path scales  $\lambda_1 \sim 0.2$  fm and  $\lambda_2 \sim 0.4$  fm

#### **Dynamics in mixtures**

$$\eta(\tau) = \frac{2}{5} \cdot e \cdot \left( \frac{r(\tau)}{1 + r(\tau)} \cdot \lambda_1^{-1} + \frac{1}{1 + r(\tau)} \cdot \lambda_2^{-1} \right)$$

$$r(\tau) = \frac{\pi_1(\tau)}{\pi_2(\tau)} = A(n, \sigma) \cdot \tanh\left(\tau \cdot B(n, \sigma) + C(n, \sigma, \pi_0)\right)$$

From the results so far we can conclude

Existence of a characteristic time-dependence of the viscosity in a mixture

Applicability of one-component hydrodynamics to a mixture depends on the chosen initial conditions

#### Initializing hydrodynamic calculations

$$\dot{\pi}^{\mu\nu} = -\frac{\pi^{\mu\nu}}{\tau_{\pi}} + \frac{\sigma^{\mu\nu}}{\beta_2} + \pi^{\mu\nu}\frac{T}{\beta_2}\partial_{\alpha}\left(\frac{\beta_2}{2\mathrm{T}}u^{\alpha}\right)$$

In one-component hydrodynamic calculations the standard choices are

$$\pi^{\mu\nu}(\tau_0) = 0 \quad \lor \quad \pi^{\mu\nu}(\tau_0) = 2 \eta \sigma^{\mu\nu}$$

...but there is no clear prescription what's the right choice. For a mixture this would mean

$$\pi_{i}^{\mu\nu}(\tau_{0}) = 0 \rightarrow \dot{\pi}_{i}^{\mu\nu}(\tau_{0}) = \frac{\sigma^{\mu\nu}}{\beta_{i}} \rightarrow \frac{\pi_{1}(\tau_{0} + d\tau)}{\pi_{2}(\tau_{0} + d\tau)} = \frac{\beta_{2}}{\beta_{1}} = \frac{e_{1}}{e_{2}} = \frac{n_{1}}{n_{2}}$$

Which also means, that the characteristic time-dependence of shear viscosity must be taken into account

#### **Conclusions and Outlook**

Standard one-component hydrodynamics in general cannot be applied to describe dissipative effects in mixtures

It is only in case the initial conditions are chosen properly that onecomponent description can be applied

Green-Kubo formalism is not reliable for mixtures – additional timemodulation must be taken into account

 $\eta/s=\eta/s(T) \rightarrow \eta/s=\eta/s(T) * f(t)$ 

# **Conclusions and Outlook**

➤ Most reliable way to check these conclusions: Kinetic transport calculations → BAMPS

See how evolution of an expanding "QGP" with  $\sigma_{gg'}$ ,  $\sigma_{gq'}$ ,  $\sigma_{qq} \sim 1/T^2$  can be reproduced by one-component calculations.

How the cross section (i.e.  $\eta/s$ ) must be chosen in one-component case? Can any hint of the time-depence of  $\eta$  be seen?

Mixture in BAMPS  $\rightarrow$  (isochronous) freeze-out  $\rightarrow$  flow observables vs One-component fluid in BAMPS  $\rightarrow$  (isochronous) freeze-out  $\rightarrow$  flow observables

Work in progress